

Parameter sheet for InterFrost Test Case TH3 "Talík Opening/Closure"

(Version 2.1, 18th Febr. 2015)

Geometrical features, boundary conditions and parameter sets are provided below as well as performance measures.

Geometrical features

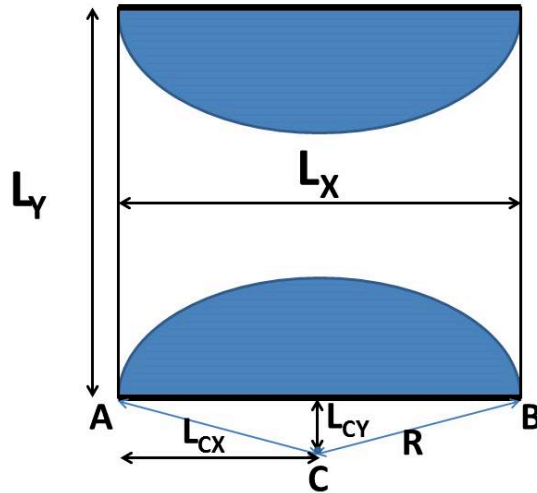


FIGURE 1 – Geometrical features : the circle centered in C goes through points A and B. $CA = CB = R$

| Symbol | Description | Value | Unit |
|--------------------|------------------------------------------------------------------|------------|----------|
| L_x | Longitudinal extension of the simulated domain | 1 | <i>m</i> |
| L_y | Lateral extension of the simulated domain | 1 | <i>m</i> |
| $(L_{cx}; L_{cy})$ | Position of the lower circle center (Symmetry for the upper one) | (0.5; 0.1) | <i>m</i> |
| R | Radius | 0.5099 | <i>m</i> |

TABLE 1 – Geometrical parameter values for TH3 Test Case

Boundary and initial conditions

Initial temperature conditions are provided in Fig. 3 : $+5^\circ\text{C}$ in the central part and -5°C in the upper and lower circular zones. This temperature field is Boolean. The initial pressure and velocity field result from a steady state flow simulation with the permeability field associated with the initial temperature field and the pressure/head boundary conditions provided in Fig. 2.

The downstream right boundary condition for heat transfer is an imposed zero conductive flux condition. This means that the heat exits the system purely by advection. Refer to Fig. 3 for conditions on other boundaries. The values of the imposed head gradient are varied in a sensitivity analysis to the advection term in the exercise (refer to Tab. 2)

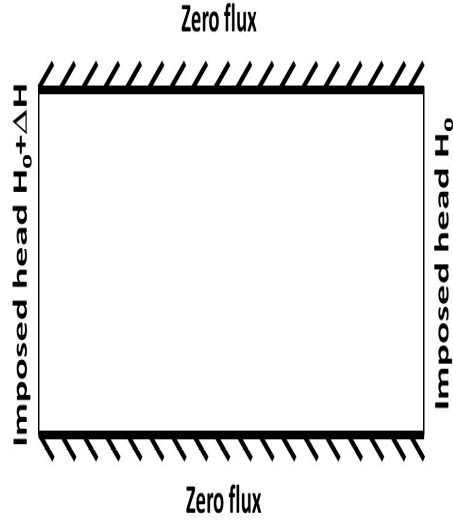


FIGURE 2 – Water flow boundary conditions

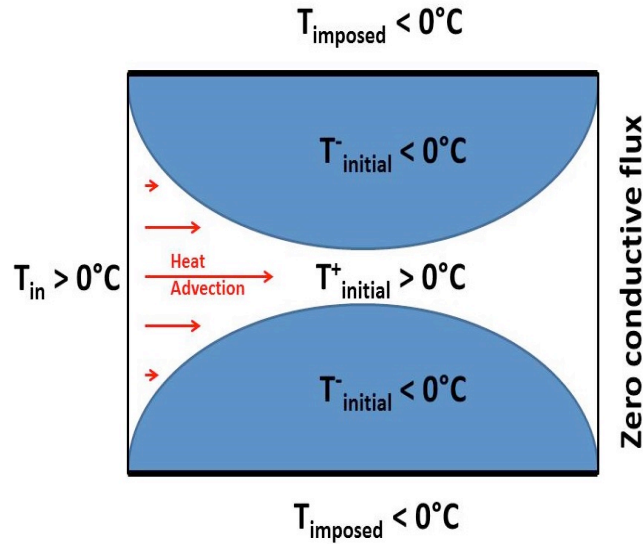


FIGURE 3 – Heat transfer boundary conditions and initial thermal conditions

| Symbol | Description | Value | Unit |
|-----------------|---------------------------------------------|-------|-------------|
| $T_{initial}^-$ | Initial temperature of the frozen inclusion | -5 | $^{\circ}C$ |
| $T_{initial}^+$ | Initial temperature of the thawed domain | +5 | $^{\circ}C$ |
| T_{in} | Temperature of the incoming flow | +5 | $^{\circ}C$ |
| $T_{imposed}$ | Imposed cold temperature | -5 | $^{\circ}C$ |
| $\Delta H/L_x$ | Hydraulic head gradient 1 | 0 | (-) |
| $\Delta H/L_x$ | Hydraulic head gradient 2 | 0.03 | (-) |
| $\Delta H/L_x$ | Hydraulic head gradient 3 | 0.09 | (-) |
| $\Delta H/L_x$ | Hydraulic head gradient 4 | 0.15 | (-) |

TABLE 2 – Initial and boundary conditions for temperature and suggested hydraulic head gradients for TH3 Test Case

Equations

Equations solved in our Cast3M code for this test case are provided here. We kindly ask participants to adopt a similar model to allow easy inter-comparison.

Flow equation (Eq. 1) :

$$(S_w \epsilon \rho_w g \beta) \frac{\partial p}{\partial t} = \vec{\nabla} \cdot (\mathbf{K}_w (\vec{\nabla} p + \vec{\nabla} z)) + \left(\epsilon \frac{\rho_i - \rho_w}{\rho_w} \frac{\partial S_w}{\partial t} \right) \quad (1)$$

Heat transfer (Eq. 2) :

$$\left(\epsilon (S_w \rho_w C_w + S_i \rho_i C_i) + (1 - \epsilon) \rho_s C_s + \epsilon \rho_i L \frac{\partial S_w}{\partial T} \right) \frac{\partial T}{\partial t} = \vec{\nabla} \cdot (\lambda_{\text{eq}} \vec{\nabla} T) + \vec{\nabla} \cdot (\rho_w C_w T \mathbf{K}_w (\vec{\nabla} p + \vec{\nabla} z)) \quad (2)$$

Subscripts denote w for water, i for ice, s for solid matrix. Unknowns are p for pressure expressed in meters ($p = P/\rho_w g$, with P pressure in Pascals) and T for temperature ($^{\circ} K$).

Please note that :

- for the sake of simplicity no dispersion term is included in the conductive term.
- still for the sake of simplicity, no temperature dependence for water density or water viscosity was introduced. The ρ_w and μ parameters in Tab. 3 are fixed values.
- compressibility β (see Tab. 3) is an equivalent value combining liquid, solid and matrix compressibility.
- considering the symmetry of the problem, one may only model the upper or lower half of the domain.

Performance measures

Performance measures for code results inter-comparison are :

- **PF1** : Plot the evolution of the equivalent permeability of the system as a function of time (the equivalent permeability results from the steady state simulation of flow and computation of total water flux divided by head gradient).
- **PF2** : Plot the evolution of the total heat flux entering the lateral boundaries (upper and lower limits where negative temperature is imposed) as a function of time.
- **PF3** : Plot the evolution of the total heat within the simulated domain as a function of time.

A parameter sensitivity study is proposed to vary flow velocities with a series of imposed head gradient values (see Tab. 2). So these performance measures should be provided for these 4 flow regimes on the same graph.

Another sensitivity study is suggested as an option. It concerns the W parameter in the $S_w(T)$ law providing larger or smaller “mushy zones”. The unique value of 0.5 is proposed in Tab. 3, corresponding to a B_t value of roughly $-1^{\circ}C$ for the linear law (see [McKenzie et al. 2007], mushy zone extends from $0^{\circ}C$ to $-1^{\circ}C$). However two other values are suggested : 1.87 corresponding roughly to a B_t of $-4^{\circ}C$ and 0.05 corresponding to a B_t value of $-0.1^{\circ}C$. These runs should be considered for the base case head gradient of 0.03. The performance measures associated with these 3 values should be plot together on a separate graph.

Parameter values

| Symbol | Description | Value or expression | Unit |
|-----------------|--------------------------------------|----------------------------------------------------------------------------|--------------------|
| ϵ | Porosity | 0.37 | (-) |
| β | Compressibility | 10^{-8} | Pa^{-1} |
| g | Acceleration of Gravity | 9.81 | $m.s^{-2}$ |
| λ_w | Water thermal conductivity | 0.6 | $W.m^{-1}.K^{-1}$ |
| λ_i | Ice thermal conductivity | 2.14 | $W.m^{-1}.K^{-1}$ |
| λ_s | Solid matrix thermal conductivity | 9 | $W.m^{-1}.K^{-1}$ |
| λ_{eq} | Equivalent thermal conductivity | $\epsilon(S_w\lambda_w + (1 - S_w)\lambda_i) + (1 - \epsilon)\lambda_s$ | $W.m^{-1}.K^{-1}$ |
| C_w | Water Heat capacity | 4182 | $J.kg^{-1}.K^{-1}$ |
| C_i | Ice Heat capacity | 2060 | $J.kg^{-1}.K^{-1}$ |
| C_s | Solid matrix heat capacity | 835 | $J.kg^{-1}.K^{-1}$ |
| ρ_w | Water volumetric mass | 1000 | $kg.m^{-3}$ |
| ρ_i | Ice volumetric mass | 920 | $kg.m^{-3}$ |
| ρ_s | Solid matrix volumetric mass | 2650 | $kg.m^{-3}$ |
| $(\rho C)_{eq}$ | Equivalent volumetric Heat capacity | $\epsilon(S_w\rho_w C_w + (1 - S_w)\rho_i C_i) + (1 - \epsilon)\rho_s C_s$ | $J.m^{-3}.K^{-1}$ |
| μ | Water dynamic viscosity | $1.793 \cdot 10^{-3}$ | $kg.m^{-1}.s^{-1}$ |
| L | Latent heat | $3.34 \cdot 10^5$ | $J.kg^{-1}$ |
| $S_w(T)$ | Water saturation for $T \geq 273.15$ | 1 | (-) |
| $S_w(T)$ | Water saturation for $T < 273.15$ | $(1 - S_{wres})e^{-((T-273.15)/W)^2} + S_{wres}$ | (-) |
| S_{wres} | Residual saturation in $S_w(T)$ | 0.05 | (-) |
| W | Parameter in $S_w(T)$ | 0.5 | K |
| K_w | Permeability | $k_r k_{int} \rho_w g / \mu$ | $m.s^{-1}$ |
| k_{int} | Intrinsic permeability | $1.3 \cdot 10^{-10}$ | m^2 |
| $k_r(S_w)$ | Relative permeability | $10^{-\Omega\epsilon(1-S_w)}$ if $k_r(S_w) > 10^{-6}$ | (-) |
| $k_r(S_w)$ | Relative permeability | 10^{-6} if $k_r(S_w) \leq 10^{-6}$ | (-) |
| Ω | Impedance factor | 50 | (-) |

TABLE 3 – Physical parameter values and expressions considered for TH3 Test Case