Monitoring and modelling groundwater flow dynamics in a glacial aquifer system with degrading & discontinuous permafrost (Umiujaq, Nunavik, Canada)

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Research sites in Canadian permafrost



Heginbottom et al. 1995

Legend (after Allard and Seguin 1987)

Sporadic permafrost

Discontinuous and

scattered permafrost

Discontinuous but

widespread permafrost

Continuous permafrost

Immatsiak network location

1 km

Study

site

IKONOS satellite image (SPACE IMAGING – July 26th 2005) Image draped on a digital elevation model Village of Umiujaq

Airpor

Hudson Bay South oblique view with artificial illumination

Vertical exaggeration 2:1

Recent climate variability and impacts



Motivation and Objectives

- Provincial Groundwater Monitoring Network
- Assess the impacts of climate change on groundwater resources (Quebec Climate Change Plan)
- Immatsiak network (meaning "source of fresh water" in Inuktitut), Umiujaq
- Study the groundwater dynamics in permafrost environments
- Hypothesis 1: Improved groundwater availability
- Hypothesis 2: Groundwater flow increases permafrost degradation



http://www.mddep.gouv.qc.ca/eau/piezo/index.htm ⁵







Drilling campaign June 2012





July 2013











Conceptual Cross-Section



Distance (m)

HEATFLOW/SMOKER Model

(Molson & Frind 2014)

- 3D Galerkin finite element
- Deformable brick elements
- PCG symmetric matrix solver
- Porous medium & discrete fractures
- Heat, mean age & mass transport
- Equilibrium geochemistry
- Liquid & ice phases, latent heat
- Picard iteration







Numerical Simulation Approach: HEATFLOW/SMOKER

Porous Matrix :

$$\frac{\partial}{\partial x_i} \left[K_{i,j}(T) \left(\frac{\partial \psi}{\partial x_j} + \rho_r(T) \cdot \overline{n}_j \right) \right] - \sum_{k=1}^N Q_k(t) \cdot \delta(x_k, y_k, z_k) = S_s \frac{\partial \psi}{\partial t}$$

$$-\frac{\partial}{\partial x_{i}}\left(\theta S_{w}c_{w}\rho_{w}v_{i}T\right) + \frac{\partial}{\partial x_{i}}\left(\overline{\lambda} + \theta S_{w}c_{w}\rho_{w}D\right)\frac{\partial T}{\partial x_{j}} + \Omega = \frac{\partial\left(C_{o}T\right)}{\partial t}$$
$$C_{o} = \theta S_{w}c_{w}\rho_{w} + \theta S_{i}c_{i}\rho_{i} + (1-\theta)c_{s}\rho_{s} + \theta\rho_{i}L\left(\frac{\partial S_{w}}{\partial T}\right)$$

 $J_{i} = \left(\frac{\lambda_{u}}{B_{z}}\right) (T_{a} - T_{s}) + (q \cdot c_{w} \rho_{w}) \cdot (T_{q} - T_{s})$

Surface b.c.:

Fractures: $\frac{-\frac{\partial(S_{w}c_{w}\rho_{w}\overline{v}_{i}T')}{\partial x_{i}} + \frac{\partial}{\partial x_{i}}\left(\overline{\lambda} + S_{w}c_{w}\rho_{w}D\frac{\partial T'}{\partial x_{j}}\right) + \frac{S_{w}c_{w}\rho_{w}D}{b}\left[\frac{\partial T}{\partial z}\right]_{z=\pm b} = \frac{\partial C_{o}T'}{\partial t}}{\int t^{2}}$ Fracture velocities: $v = \frac{-(2b)^{2}}{12\mu}\rho_{g}\nabla h$

Fluid Viscosity and Density Functions:

Frozen/Unfrozen Water:



$$k_r = \max\left[\left(\frac{Wu(T) - p}{1 - p}\right)^4, \ 10^{-6}\right]$$



The Borden Thermal Injection Experiment HEATFLOW/3D Simulation

(see Molson et al., Water Resour, Res., 28 (10), 2857-2867, 1992)



Conceptual Cross-Section



Distance (m)

Permafrost Evolution: Umiujaq Temperature & flow lines



Permafrost Evolution: Umiujaq Temperature & flow lines



20 m

Acknowledgements

Développement durable, Environnement et Lutte contre les changements climatiques





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Program of Energy Research and Development (PERD) Indian & Northern Affairs Canada (INAC)

Model Benchmarks

HEATFLOW/SMOKER Model



Distance (m)

11.6

Model Benchmarks:

HEATFLOW/SMOKER Model

Validation: Lunardini (1985) 3-zone solution programmed by M. Ghias, U. Laval





Benchmark TH2 SMOKER Model (Molson & Frind, 2014)







Benchmark TH2 SMOKER Model (Molson & Frind, 2014)





Benchmark TH2 SMOKER Model (Molson & Frind, 2014)







0.00 days



4.5 3.5

2.5 1.5 0.5 -0.5

0.00 days





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Fonds de recherche Nature et technologies







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Program of Energy Research and Development (PERD) Indian & Northern Affairs Canada (INAC)

Validation: Stallman (1965) Solution


Validation: Discrete Fractures



Umiujaq Model: Permafrost Hydrogeology

HEATFLOW/SMOKER Model



Umiujaq Isotope Data 2013-2014



Permafrost Evolution: Umiujaq Temperature & flow lines

20 m



Black Smoker Simulation Smoker Heat Transport Model



Fracture Network



Simulated Temperature Distributions (2b=500µm)



Simulated Subsurface Temperature Profiles

Heatflow model (Molson & Frind, 2009)



Benchmark TH3 SMOKER Model (Molson & Frind 2014)











200 days



Groundwater – Surface Water Interaction: Use of thermal regimes to quantify contaminant discharge



HEATFLOW Model: 3D Ice Wall Numerical Simulation





Hydrodynamic Dispersion vs. Thermal Diffusivity







Le pergélisol: quelques concepts (profil thermique, définitions du pergélisol et du mollisol)



Deuxième exemple d'un bassin versant à Umiujaq (investigation hydrogéologique: campagne de forages à l'été 2012)





Deuxième exemple d'un bassin versant à Umiujaq (investigation cryohydrogéophysique: coupe hydrostratigraphique interprétative)



amera and Voice

Deuxième exemple d'un bassin versant à Umiujaq (investigation hydrogéologique: coupe cryohydrostratigraphique interprétative)



Numerical simulation of coupled groundwater flow and heat transport in a continuous permafrost environment : Iqaluit, Canada

Masoumeh Shojae Ghias, René Therrien, John Molson, Jean-Michel Lemieux Université Laval, Quebec City, Canada



Study site: Iqaluit airport

Permafrost map of Canada Heginbottom et al. 1995 Continuous (90-100%) other lar Extensive Discontinuous (50-90%) Isolated Patches (<10%) Alpine Permafrost Only Subsea Permafrost Sporadic Discontinuous No Permafrost

Iqaluit airport



- Latitude of 63°45' N
- Continuous permafrost
- Mean Annual T: -7.76 C

Current Issues at Iqaluit airport







Frost cracks



Depressions



Concrete patch



Site investigation at Iqaluit airport

Surface and subsurface geology

- Drilling, coring
- Geophysical survey
- Lab analysis

Climate related data

- Surface and subsurface T
- Snow depth

Ground movement



Conceptual Geological Cross-section



Vertical exageration 10x

HEATFLOW-SMOKER MODEL(Molson et al. 2012)

- 3D finite element
- Freezing and thawing and latent heat
- Partially saturated zone for thermal transport
- Coupled density dependent flow and thermal transport

Validation of HEATFLOW-SMOKER

 Numerical vs. analytical model (Lunardini, 3-zone freezing-front problem)





Fracture Network

Coupled heat-fluid flow model

1. Calibration



2. Designed scenarios

SR-1.Saturated vs. unsaturated
SR-2.Advection-conduction vs. conduction heat transport
SR-3.Heterogeneous hydraulic conductivity distribution



Starting point for all the designed scenarios



Model calibration

Temperature for the last year of simulation for 1971-2012



Sensitivity Analysis



Future climate warming scenarios

• Data from GCM (AR4, IPCC 2007)

• SR-B1, SR-A1B, SR-A2 (low, medium and high greenhouse gas emission scenario)

• Time period: 2071-2100

• Downscale method : Delta change

Sr-1: effects of saturated vs unsaturated on permafrost



SR-1: Comparison of completely saturated and partly unsaturated model on permafrost thaw under future climate warming

Result Plotted for the last September of each warming period



SR-1. Temperature changes as a function of time at a

2.5 m depth



Conclusion

- ✓ Calibration of simplified 2D model
 - ✓ Best for Winter months
 - ✓ Greater difference for spring and early summer

✓ Key parameter : thermal conductivity of the uppermost soil layer

✓ **Saturated** vs. unsaturated upper zone

- ✓ Differences are greater for negative temperatures at surface
- ✓ Active layer expands faster under the same climate warming
- ✓ Deeper permafrost table

Ongoing work

SR-2. Conductive vs advective conductive model

Conduction model

Conduction-advection model


Ongoing work

SR-3. Effects of heterogeneous hydraulic conductivity on permafrost

Natural layer



 $K = 10^{-12} - 10^{-3}$ (m/sec)

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CENTRE D'ÉTUDES NORDIQUES

CEN Centre for Northern Studies























Permafrost in Northern Québec



Immatsiak network location

IKONOS satellite image (SPACE IMAGING – July 26th 2005) Image draping on a digital elevation model South oblique view with artificial illumination

Vertical exaggeration 2:1

Le pergélisol: quelques concepts

(types d'aquifère en régions nordiques et talik ouvert ou fermé)



Site Description



Wells location Satellite image

Basic site investigation











Hydrocarbon Contamination in Fractured Rock at the Colomac Mine Site, NWT





Environment Canada





J. W. Molson

Canada Research Chair, Quantitative Hydrogeology of Fractured Porous Media Géologie & Génie Géologique Université Laval, Quebec City



7th International Conference **Contaminants in Freezing Ground**

May 24-28, 2010 Kingston, Ontario, Canada



Interest in Northern Hydrogeology

- Guidance on petroleum impacts in Canadian North
- Expanding resource activity & contaminated sites legacy
- Hydrogeological knowledge gap in cold-climate regions
- Role of permafrost & seasonal active layer on groundwater



Colomac Mine (2005)

Colomac Mine

Yellowknife

Ottawa

Quebec City

Kingston

Modified after Google Earth (2007)

Canadian Permafrost Zones



Colomac Mine

(looking south circa 1997)

Steeves Lake

1990 4000L

Gasoline

Diesel Study

1997: 27 276L Diesel

Machine Shop

Tank Farm

Mill

Free-Phase
 Discharge

Camp

Photo Courtesy of INAC

Objectives

- Characterize fractured bedrock permeability & contaminant distribution
- Document dynamics of subsurface thermal regime
- Explore geochemical evidence for intrinsic bioremediation
- Refine conceptual model of local groundwater system





Colomac Mine (2005)

Monitoring Network

- 33 bedrock monitoring boreholes
- 10 thermistor arrays to 15 m depth
- 3 thermistor arrays at base of barrier wall



Subsurface Temperature Profiling

Thermistor array

TAXABLE INCOME.



Barrier Wall

BH15

Steeves Lake

Subsurface Temperature Profiling



April 12, 2006 to March 30, 2007



Numerical Simulation Approach:

HEATFLOW/SMOKER Model (Molson & Frind 2009)

3D Porous Matrix:

$$\frac{\partial}{\partial x_i} \left[\left(\kappa + \frac{D_{ij}}{R} \right) \frac{\partial T}{\partial x_j} \right] - \frac{\partial}{\partial x_i} \left(\frac{v_i}{R} T \right) = \frac{\partial T}{\partial t}$$
2D Fractures:

$$\frac{\partial}{\partial x_i} \left(D'_{ij} \frac{\partial T'}{\partial x_j} \right) - \overline{v_i} \frac{\partial T'}{\partial x_i} - \frac{D'_{ij}}{b} \left[\frac{\partial T'}{\partial z} \right]_{z=\pm b} = \frac{\partial T'}{\partial t}$$
Fracture
velocities:

$$\overline{v} = \frac{-(2b)^2}{12\mu} \rho_g \nabla h$$

Natural Thermal Source Model



Flow Simulation

Steady State Hydraulic Head



Simulated Temperature Distributions (2b=500µm)



Heatflow Simulation: Surface Temperature Source

0.00 days_'s


Simulated Subsurface Temperature Profiles

Heatflow model (Molson & Frind, 2009)



Simulated temperature profiles: Colomac site

Conduction only, no flow



Time (days)

HEATFLOW Model: 3D Ice Wall Numerical Simulation



Groundwater Geochemistry

- Discrete samples from features identified in permeability profiling
- Petroleum impacts in most wells
- Uniform inorganic chemistry observed
- Volatile fatty acids suggest intrinsic bioremediation occurring



Substrate/Electron Acceptor/Microbe Coupling BIONAPL / 3D

$$\frac{\partial C^{\alpha}}{\partial t}R = \frac{\partial}{\partial x_i} \left[D_{ij} \frac{\partial C^{\alpha}}{\partial x_j} \right] - v_i \frac{\partial C^{\alpha}}{\partial x_i} + \lambda^{\alpha}_{DIS} \left(C_S - C^{\alpha} \right) - \lambda^{\alpha}_{BIO} C^{\alpha}$$





Simulated Gasoline Spill Heterogeneous Porous medium: Realization 5

50 days

100 days



Simulated Gasoline Spill Fractured Porous Medium

Initial Condition + Fracture Network





Colomac Conceptual Model: Aqueous Phase Petroleum Hydrocarbons



Summary

- Seasonal dimension to groundwater system but deeper portions always active
- Absence of permafrost above 15 m depth
- Indicators of intrinsic bioremediation present





Colomac Mine (2007)

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Natural Sciences and Engineering Research Council of Canada

